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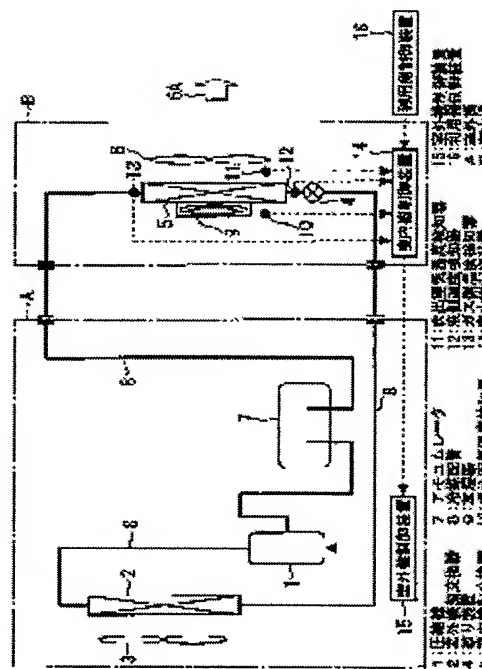
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(54) AIR CONDITIONER

(57)Abstract:

PROBLEM TO BE SOLVED: To solve problems in a vapor pan type humidifier usually used in performing cooling and air conditioning throughout the year where humidifying capacity decreases when a maintenance is not performed periodically, the inside of the humidifier gets soiled, and electric power is always required.

SOLUTION: This air conditioner comprises an outdoor machine A and an indoor machine B. The outdoor machine A comprises a compressor 1, an outdoor machine heat exchanger 2 for condensing and liquefying gas refrigerant delivered from the compressor, and an accumulator 7 connected to the suction side of the compressor. The indoor machine B comprises a throttle device 4 for decompressing liquefied refrigerant from the outdoor machine heat exchanger 2, an indoor machine heat exchanger 5 disposed in a predetermined air duct on the use side for evaporating and gasifying the refrigerant decompressed by the throttle device 4, and making the refrigerant flow into the accumulator, and a natural evaporation type humidifier 9 disposed on the primary side of the air duct 6A of the indoor machine heat exchanger.



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CLAIMS

[Claim(s)]

[Claim 1]A conditioner provided with an interior unit characterized by comprising the following.
A compressor.

An exterior unit heat exchanger which condensate-izes a gas refrigerant breathed out from this compressor.

An exterior unit which has the accumulator connected to an inlet side of the above-mentioned compressor, and an collimator which decompresses a liquefied refrigerant from the above-mentioned exterior unit heat exchanger.

An interior unit heat exchanger which is a use side, is allocated all over a predetermined air course, evaporates a refrigerant decompressed by the above-mentioned collimator, gasifies, and is made to flow into the above-mentioned accumulator, and a natural vaporization type humidifier formed in a primary side of an air course of the above-mentioned interior unit heat exchanger.

[Claim 2]The conditioner according to claim 1, wherein the above-mentioned interior unit heat exchanger is allocated so that a refrigerant inlet may be located in the downstream of an air course and a refrigerant exit may be located in a primary side of an air course.

[Claim 3]The conditioner according to claim 1 or 2 making a pipe supplementary biography hot surface product of the above-mentioned interior unit heat exchanger large to such an extent that sufficient refrigeration capacity is securable, even if evaporating temperature is high.

[Claim 4]A conditioner of claim 1 using the above-mentioned compressor as a capacity variable type compressor - claim 3 given in any 1 paragraph.

[Claim 5]The conditioner according to claim 4 provided with a control device which carries out capacity control of the compressor so that the liquid side temperature of the above-mentioned interior unit heat exchanger may turn into more than prescribed temperature.

[Claim 6]The conditioner according to claim 5, wherein the above-mentioned prescribed temperature is the dew-point temperature.

[Claim 7]The conditioner according to claim 6 characterized by making it the above-mentioned dew-point temperature make a solution temperature degree lower limit computed by deducting constant temperature from suction air temperature of an interior unit heat exchanger correspond.

[Claim 8]The conditioner according to claim 6 computing the above-mentioned dew-point temperature based on suction air temperature and humidity of an interior unit heat exchanger.

[Claim 9]A conditioner provided with one set of an interior unit characterized by comprising the following, and a natural vaporization type humidifier formed in a primary side of an air course of each above-mentioned interior unit heat exchanger.

A compressor.

An exterior unit heat exchanger which condensate-izes a gas refrigerant breathed out from this compressor.

The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to an inlet side of the above-mentioned compressor, respectively, and decompress liquid cooling intermediation.

A blowing means which forms an air course for heat exchange to the 1st and 2nd interior unit heat exchangers that evaporate a refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into an accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, and each above-mentioned interior unit heat exchanger.

[Claim 10]A conditioner provided with a control device which controls more highly than evaporating temperature of the 2nd interior unit heat exchanger evaporating temperature of one set of an interior unit characterized by comprising the following, a natural vaporization type humidifier formed in a primary side of an air course of an interior unit heat exchanger of the above 1st, and an interior unit heat exchanger of the above 1st.

A compressor.

An exterior unit heat exchanger which condensate-izes a gas refrigerant breathed out from this compressor.

The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to an inlet side of the above-mentioned compressor, respectively, and decompress liquid cooling intermediation.

A blowing means which forms an air course for heat exchange to the 1st and 2nd interior unit heat exchangers that evaporate a refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into an accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, and each above-mentioned interior unit heat exchanger.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Field of the Invention]This invention relates to the conditioner which performs air conditioning air conditioning through every year like a conditioner, especially a computer room.

[0002]

[Description of the Prior Art]Since the compressor of the annual air conditioning conditioner in the conventional computer room was fixed capacity, it performed reheating at the time of low loading, and was performing capability adjustment. In order to be accompanied by excessive dehumidification in that case, the humidifier of the vapor bread method of the common knowledge which humidifies compulsorily because of humidity control was used.

[0003]

[Problem(s) to be Solved by the Invention]Since electric power was always needed in the conventional conditioner which humidifies compulsorily with a vapor bread method, there was a problem that power consumption increased. By a vapor bread method, when not maintained periodically, there was a problem that the fall of humidifying capacity and the inside of a conditioner became dirty. Power consumption was unnecessary as a humidifier, though the natural vaporization type humidifier with easy cleaning was used, since the temperature of the air which passes a natural vaporization type humidifier was low, sufficient humidifying capacity could not be demonstrated but utilization was difficult.

[0004]An object of this invention is to obtain the conditioner which can use a natural vaporization type humidifier efficiently by the capacity control of a compressor, when it was made in order to solve the above problems, and performing air conditioning air conditioning through every year.

[0005]

[Means for Solving the Problem]An exterior unit heat exchanger which condensate-izes a gas refrigerant in which a conditioner concerning this invention was breathed out from a compressor and this compressor, An exterior unit which has the accumulator connected to an inlet side of a compressor, and an collimator which decompresses a liquefied refrigerant from an exterior unit heat exchanger, It is a use side and is allocated all over a predetermined air course, and a refrigerant decompressed by an collimator is evaporated, and it gasifies, and has an interior unit which has an interior unit heat exchanger made to flow into an accumulator, and the natural vaporization type humidifier formed in a primary side of an air course of this interior unit heat exchanger.

[0006]A conditioner concerning this invention is allocated so that a refrigerant inlet of an interior unit heat exchanger may be located in the downstream of an air course and a refrigerant exit may be located in a primary side of an air course again.

[0007]Even if evaporating temperature is high, the conditioner concerning this invention enlarges a pipe supplementary biography hot surface product of an interior unit heat exchanger again to such an extent that it can secure sufficient refrigeration capacity.

[0008]A conditioner concerning this invention uses a compressor as a capacity variable type compressor again.

[0009]A conditioner concerning this invention is provided with a control device which carries out capacity control of the compressor again so that the liquid side temperature of an interior unit heat exchanger may turn into more than prescribed temperature.

[0010]A conditioner concerning this invention makes prescribed temperature the dew-point temperature again.

[0011]It is made for a conditioner concerning this invention to make a solution temperature degree lower limit computed again by deducting constant temperature from suction air temperature of an interior unit heat exchanger as the dew-point temperature correspond.

[0012]A conditioner concerning this invention computes the dew-point temperature based on suction air temperature and humidity of an interior unit heat exchanger.

[0013]A conditioner concerning this invention A compressor and an exterior unit heat exchanger which condensate-izes a gas refrigerant breathed out from this compressor, The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to an inlet side of a compressor, respectively, and decompress liquid cooling intermediation, The 1st and the 2nd interior unit heat exchanger which evaporate a refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into an accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, It has one set of an interior unit which has a blowing means which forms an air course for heat exchange to each interior unit heat exchanger, and a natural vaporization type humidifier formed in a primary side of an air course of each interior unit heat exchanger.

[0014]A conditioner concerning this invention A compressor and an exterior unit heat exchanger which condensate-izes a gas refrigerant breathed out from this compressor, The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to an inlet side of a compressor, respectively, and decompress liquid cooling intermediation, The 1st and the 2nd interior unit heat exchanger which evaporate a refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into an accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, One set of an interior unit which has a blowing means which forms an air course for heat exchange to each interior unit heat exchanger. It has a control device which controls more highly than evaporating temperature of the 2nd interior unit heat exchanger evaporating temperature of a natural vaporization type humidifier formed in a primary side of an air course of the 1st interior unit heat exchanger, and the 1st interior unit heat exchanger.

[0015]

[Embodiment of the Invention]Below embodiment 1. describes this embodiment of the invention 1 based on figures. Drawing 1 is a refrigerant circuit figure showing the composition of Embodiment 1. In this figure, A is an exterior unit and is constituted by each device described below. That is, it is the interior unit blowing means by which provide the exterior unit blowing means by which the compressor of a capacity variable type [1] and 2 were provided in the exterior unit heat exchanger, and 3 was provided in the exterior unit heat exchanger 2, and 4 in an collimator, 5 was provided in the interior unit heat exchanger, and 6 was provided in the interior unit heat exchanger 5, and the air course shown by the arrow 6A at the time of operation is formed. The refrigerant piping which 7 connects an accumulator, and 8 connects each above-mentioned device in series in above order, and constitutes a refrigerant circuit, The natural vaporization-type humidifier with which 9 was provided in the primary the air course 6A of the interior unit heat exchanger 5 side, The sink air-temperature detector in which 10 was provided in the suction side (primary side) of the air course of the interior unit heat exchanger 5, The blow-off air-temperature detector in which 11 was similarly provided in the blow-off side (secondary), The liquid side temperature detector in which 12 was provided near the entrance of the interior unit heat exchanger 5, the gas side temperature detector in which 13 was similarly provided near the exit, An interior unit control device which controls the interior unit B with which 14 contains the collimator 4 based on the detection result of each above-mentioned temperature detector, They are an exterior unit control device which 15 is provided in the

exterior unit A and carries out capacity control of the compressor 1, and a use side control device which 16 is provided in the use side and controls the interior unit control device 14 and the exterior unit control device 15.

[0016]Next, it explains that the refrigerant of the conditioner of Embodiment 1 flows. The hot and high-pressure gas refrigerant breathed out from the compressor 1 flows into the exterior unit heat exchanger 2, and it is cooled by the air etc. of ordinary temperature including air blasting of the exterior unit blowing means 3, and it is condensate-ized. The refrigerant which came out of the exterior unit heat exchanger 2 is decompressed with the collimator 4, and flows into the interior unit heat exchanger 5. Low temperature is generated in the interior unit heat exchanger 5, and a refrigerant evaporates, is gasified and flows out, a gas refrigerant flows into the accumulator 7, and after passing, it is inhaled to the compressor 1.

[0017]Next, control of the collimator 4 is explained using the flow chart of drawing 2. First, the superheating SH (= TH2-TH1) which is a difference of detection temperature TH1 of the liquid side temperature detector 12 of the interior unit heat exchanger 5 and detection temperature TH2 of the gas side temperature detector 13 is computed at Step S1. Next, it is judged whether the collimator 4 is extracted by size comparison with the superheating SH and the target superheating value SHm at Step S2, or it opens. In $SH > SHm$, the amount Sj2 of difference of the collimator 4 (SH) is computed at Step S3, and only Sj2 (SH) opens the collimator 4 by step S4 in it. In $SH < SHm$, the amount Sj1 of diaphragms of the collimator 4 (SH) is computed at Step S5 by Step S2, and only Sj1 (SH) extracts the collimator 4 at Step S6.

[0018]Next, the humidifier 9 is explained. The humidifier 9 adopts the humidification method of the natural vaporization type containing the **** film type which does not need an electric power supply, and humidifying performance changes with the temperature of the air which passes the humidifier 9, humidity, and air capacity. That is, since humidifying performance improves, and humidifying performance falls when reverse so that it is an elevated temperature, damp, and large air capacity, humidity control can be performed automatically. Since the air which passes the humidifier 9 will turn into air of low-temperature high humidity and a humidity effect will fall dramatically here if the humidifier 9 is installed in the secondary of the air course 6A of the interior unit heat exchanger 5, in Embodiment 1. He installs a humidifier in a primary the air course 6A of the interior unit heat exchanger 5 side, and is trying for the air which passes the humidifier 9 to turn into interior unit sink air with it. [a high temperature and] [damp] In this way, the air humidified with the humidifier 9 is cooled by the interior unit heat exchanger 5, and blows off to interior space. When the liquid side temperature of the interior unit heat exchanger 5 is lower than the dew-point temperature of the air humidified with the humidifier at this time, Since a part is condensed and it is dehumidified, it enables it to supply humidity to interior space by carrying out capacity control of the compressor 1, without being dehumidified, as the liquid side temperature becomes higher than the dew-point temperature.

[0019]Although the natural vaporization type humidifier 9 has a humidifying amount smaller than the humidifier of a compulsive formula, since dehumidification volume can be small stopped with the compressor 1 in which capacity control is possible, excessive humidification becomes unnecessary. Since especially the open air indoors introduced by ventilation in the summer or the interphase is humid, humidification is unnecessary. In winter, since the open air indoors introduced by ventilation has low humidity, humidification is needed, but in object air conditioning, such as a computer room, since there are few persons in the interior of a room for air conditioning, there may be few amounts of ventilation and the humidifying amount of a natural vaporization type humidifier is also enough as them.

[0020]Next, a control flow of the compressor 1 is explained using drawing 3. Blow-off air-temperature TH4 which blew off with target temperature TH4m of the blow-off air temperature set up by the use side control device 16 at Step S11, and was detected in the air-temperature detector 11 is compared. When TH4 is larger, desired value TH1m of the liquid side temperature of the interior unit heat exchanger 5 is made small at Step S12, and when TH4 is smaller, TH1m is enlarged at Step S13. Next, detection temperature TH3 of the interior unit sink air-temperature detector 10 and prescribed temperature, for example, a difference with 12 **, are computed at Step S14 as liquid side temperature lower limit TH1LMT (=TH3-12) corresponding

to the dew-point temperature. When TH1m is smaller than TH1LMT, it is made to be set to TH1m=TH1LMT at Step S16 by Step S15. At Step S17, when detection temperature TH1 of the liquid side temperature detector 12 of an interior unit heat exchanger is larger than TH1m, Frequency of the compressor 1 is enlarged at Step S18, capacity is increased, when TH1 is smaller than TH1m, frequency of the compressor 1 is made small at Step S19, and capacity is made small.

[0021] Since the capacity of the compressor 1 is small controlled at the time of low loading, evaporating temperature becomes high and a sensible heat factor is operated in the state of 1. Although the capacity of the compressor 1 is greatly controlled at the time of a heavy load and evaporating temperature becomes low, if it is not humid environment, there is little dehumidification volume. In order to raise the humidity effect of the humidifier 9, it is necessary to raise evaporating temperature and to operate. Thus, it is possible to set dehumidification volume in the interior unit heat exchanger 5 to 0 by performing capacity control of the compressor 1 so that the liquid side detection temperature with the lowest temperature may become higher than the dew-point temperature in the interior unit heat exchanger 5.

[0022] In order to make target solution temperature degree TH1m higher than near the dew-point temperature or it as mentioned above, were made to control by Embodiment 1 considering solution temperature degree lower limit TH1LMT computed as interior unit sink air-temperature-12 as a temperature corresponding to the dew-point temperature, but. It absorbs using a humidity sensor, the dew-point temperature is computed from an air-temperature detection value and a humidity detection value, and it may be made to control the value as a degree of target solution temperature.

[0023] Even if evaporating temperature is high, cooling capacity can make it possible to fully secure the capacity of the interior unit heat exchanger 5 greatly by setting up a pipe supplementary biography hot surface product more than 70-m^2 per 28 kW of refrigeration capacity.

[0024] Even if evaporating temperature is high, cooling capacity can make it possible to fully secure also by setting the refrigerant path of the interior unit heat exchanger 5 so that it may be made for the refrigerant inlet side to be located in the secondary of the air course 6A of a heat exchanger and the refrigerant exit side may be located in a primary the air course 6A side.

[0025] Embodiment 2., next this embodiment of the invention 2 are described based on figures. Drawing 4 is a refrigerant circuit figure showing the composition of Embodiment 2. In this figure, identical codes are given to a portion the same as that of drawing 1, or considerable, and explanation is omitted. A different point from drawing 1 is a point which is constituted by one set of two sets of exterior units, and the interior unit which has two interior unit heat exchangers corresponding to each exterior unit, and formed two refrigerant circuits. That is, the 1st refrigerant circuit 100 is considered as the same composition as drawing 1 except the point that the interior unit heat exchanger of the interior unit B turns into the 1st interior unit heat exchanger 5. The 2nd refrigerant circuit 100S is considered as the same composition as the 1st refrigerant circuit 100 except the point that the humidifier 9 is not formed in the 2nd interior unit heat exchanger 5S of the interior unit B. The numerals of each device which constitutes the 2nd refrigerant circuit 100S add and show S to the numerals of the device with which the 1st refrigerant circuit 100 corresponds, and each explanation is omitted. The 1st of the interior unit B and the 2nd interior unit heat exchanger 5 and 5S are allocated in general in V type, and the interior unit blowing means 6 is absorbed in the upper part of the mid-position of both the interior unit heat exchangers 5 and 5S, and is established as a mold fan, and it is made to have an air course like the arrow 6A or 6AS formed like a graphic display.

[0026] Next, it explains that the refrigerant of Embodiment 2 flows. Since the flow of the refrigerant of the 1st and 2nd refrigerant circuits 100 and 100S is the same, only the 1st refrigerant circuit 100 is explained. The hot and high-pressure gas refrigerant breathed out from the compressor 1 flows into the exterior unit heat exchanger 2, and it is cooled by the air etc. of ordinary temperature including air blasting of the exterior unit blowing means 3, and it is condensate-ized. The refrigerant which came out of the exterior unit heat exchanger 2 is

decompressed with the collimator 4, and flows into the 1st interior unit heat exchanger 5. Low temperature is generated in the 1st interior unit heat exchanger 5, and a refrigerant evaporates, is gasified and flows out, a gas refrigerant flows into the accumulator 7, and after passing, it is inhaled to the compressor 1.

[0027]About control of the collimator 4, since the 1st and 2nd refrigerant circuit is the same as that of Embodiment 1, it omits explanation. Although allocated by only the 1st interior unit heat exchanger 5 about the humidifier 9, since the function is the same as that of Embodiment 1, explanation is omitted.

[0028]Next, a control flow of the compressor 1 is explained. Since it is the same as that of Embodiment 1 about the 1st refrigerant circuit 100, explanation is omitted, and a control flow of the compressor of the 2nd refrigerant circuit 100S is explained using drawing 5. Blow-off air-temperature TH4 which blew off with the value lower 1 ** than target temperature TH4m of the blow-off air temperature set up by the use side control device 16 at Step S21, and was detected in the air-temperature detector 11 is compared. When TH4 is larger, desired value TH1m of the liquid side temperature of the 2nd interior unit heat exchanger 5S is made small at Step S22, and when TH4 is smaller, TH1m is enlarged at Step S23. Detection temperature TH3 of an interior unit sink air-temperature detector and prescribed temperature, for example, a difference with 12 **, are computed as liquid side temperature TH1LMT (= TH3-12) corresponding to the dew-point temperature. When TH1m is smaller than TH1LMT, it is made to be set to TH1 m=TH1LMT at Step S26 by Step S25. At Step S27, when detection temperature TH1 of the liquid side temperature detector 12S of an interior unit heat exchanger is larger than TH1m, Frequency of the compressor 1S is enlarged at Step S28, capacity is increased, when TH1 is smaller than TH1m, frequency of the compressor 1S is made small at Step S29, and capacity is made small.

[0029]The 1st refrigerant circuit 100 and 2nd refrigerant circuit 100S, By only Steps S21 in drawing 5 differing, and reading low the target temperature of the 2nd refrigerant circuit 100S in which the humidifier is not formed rather than the 1st refrigerant circuit 100 in which the humidifier 9 is formed, As a result of controlling the capacity of the compressor 1S small rather than the 1st refrigerant circuit 100, evaporating temperature of the 2nd interior unit heat exchanger 5S of the 2nd refrigerant circuit 100S can be made high, and the humidity effect of the humidifier 9 can be raised. Since the capacity of a compressor is small controlled at the time of low loading, evaporating temperature becomes high and a sensible heat factor is operated in the state of 1.

[0030]Thus, it is possible to set dehumidification volume in an interior unit heat exchanger to 0 by performing capacity control of a compressor so that the liquid side detection temperature with the lowest temperature may become higher than the dew-point temperature in an interior unit heat exchanger.

[0031]In order to make target solution temperature degree TH1m higher than near the dew-point temperature or it, were made to control by Embodiment 2 considering solution temperature degree lower limit TH1LMT computed as interior unit sink air-temperature-12 as a temperature corresponding to the dew-point temperature, but. Using a humidity sensor, the dew-point temperature may be computed from a sink air-temperature detection value and a humidity detection value, and the value may be controlled as a degree of target solution temperature.

[0032]Even if evaporating temperature is high, cooling capacity can make it possible to fully secure the capacity of an interior unit heat exchanger greatly by setting up a pipe supplementary biography hot surface product more than 70-m² per 28 kW of refrigeration capacity.

[0033]Even if evaporating temperature is high, cooling capacity can make it possible to fully secure also by setting the refrigerant path of an interior unit heat exchanger so that it may be made for the refrigerant inlet side to be located in the secondary of the air course of a heat exchanger and the refrigerant exit side may be located in a primary air course side.

[0034]Although Embodiment 2 explained the case where two refrigerant circuits were constituted, the same effect is expectable even if it constitutes three or more refrigerant circuits.

[0035]

[Effect of the Invention]The exterior unit heat exchanger which condensate-izes the gas refrigerant in which the conditioner concerning this invention was breathed out from a compressor and this compressor, An exterior unit which has the accumulator connected to the inlet side of a compressor, and an collimator which decompresses the liquefied refrigerant from an exterior unit heat exchanger, The interior unit heat exchanger which is a use side, is allocated all over a predetermined air course, evaporates the refrigerant decompressed by the collimator, gasifies, and is made to flow into an accumulator, Since it has an interior unit which has the natural vaporization type humidifier formed in the primary side of the air course of this interior unit heat exchanger, it can humidify by low power consumption and simple maintenance.

[0036]The conditioner concerning this invention Since it has the refrigerant path shape allocated so that the refrigerant inlet of an interior unit heat exchanger might be located in the downstream of an air course and a refrigerant exit might be located in the primary side of an air course, Evaporating temperature of an interior unit heat exchanger can be made high, without spoiling cooling capacity, and a humidifier can be used efficiently.

[0037]Since the conditioner concerning this invention uses a compressor as a capacity variable type compressor, it can be humidified by low power consumption and simple maintenance.

[0038]Since the conditioner concerning this invention is provided with the control device which carries out capacity control of the compressor so that the liquid side temperature of an interior unit heat exchanger may turn into more than prescribed temperature, it can make high evaporating temperature of an interior unit heat exchanger, and a humidifier can be efficiently used for it.

[0039]The conditioner concerning this invention A compressor and the exterior unit heat exchanger which condensate-izes the gas refrigerant breathed out from this compressor, The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to the inlet side of a compressor, respectively, and decompress liquid cooling intermediation, The 1st and the 2nd interior unit heat exchanger which evaporate the refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into the accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, Since it has one set of the interior unit which has a blowing means which forms the air course for heat exchange to each interior unit heat exchanger, and the natural vaporization type humidifier formed in the primary side of the air course of each interior unit heat exchanger, it can humidify by low power consumption and simple maintenance.

[0040]The conditioner concerning this invention A compressor and the exterior unit heat exchanger which condensate-izes the gas refrigerant breathed out from this compressor, The 1st and 2nd collimators that are connected to two sets of exterior units and each exterior unit which have the accumulator connected to the inlet side of a compressor, respectively, and decompress liquid cooling intermediation, The 1st and the 2nd interior unit heat exchanger which evaporate the refrigerant which was connected to the 1st and 2nd collimator, respectively and was decompressed, gasify, make it flow into the accumulator of each exterior unit, respectively, and constitute two refrigerant circuits, One set of the interior unit which has a blowing means which forms the air course for heat exchange to each interior unit heat exchanger. In order to have a control device which controls more highly than the evaporating temperature of the 2nd interior unit heat exchanger the evaporating temperature of the natural vaporization type humidifier formed in the primary side of the air course of the 1st interior unit heat exchanger, and the 1st interior unit heat exchanger, Evaporating temperature of an interior unit heat exchanger can be made high, and a humidifier can be used efficiently.

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1]It is a refrigerant circuit figure showing the composition of this embodiment of the invention 1.

[Drawing 2]It is a control flow chart figure in this embodiment of the invention 1.

[Drawing 3]It is a flow chart figure showing a control flow of the compressor in this embodiment of the invention 1.

[Drawing 4]It is a refrigerant circuit figure showing the composition of this embodiment of the invention 2.

[Drawing 5]It is a flow chart figure showing a control flow of the compressor of the 2nd refrigerant circuit in this embodiment of the invention 2.

[Description of Notations]

1 A compressor and 2 An exterior unit heat exchanger, 4 collimators, and 5 Interior unit heat exchanger, 7 An accumulator, 8 refrigerant piping, nine humidifiers, and 10 [The gas side temperature detector and 14 / An interior unit control device and 15 / An exterior unit control device, 16 use side control device, A exterior unit, and B / Interior unit.] A suction air-temperature detector and 11 A blowing off air temperature detector and 12 The liquid side temperature detector and 13

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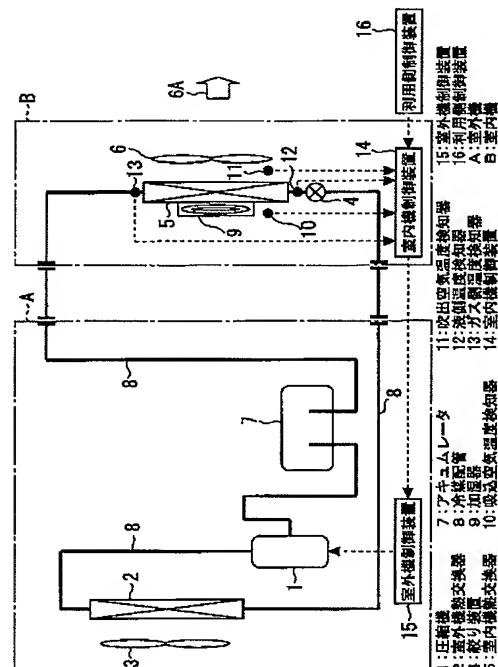
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(54) 【発明の名称】 空気調和装置

(57) 【要約】

【課題】 年間を通じて冷房空調を行なう場合に、通常用いられているペーパーパン方式の加湿器は、定期的にメンテナンスを実施しないと加湿能力が低下し、装置の内部が汚れる他、常に電力を必要とするという問題点があった。

【解決手段】 圧縮機1と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器2と、圧縮機の吸入側に接続されたアキュムレータ7とを有する室外機A、及び室外機熱交換器2からの液化冷媒を減圧する絞り装置4と、利用側で所定の風路中に配設され、絞り装置4によって減圧された冷媒を蒸発させてガス化し、アキュムレータに流入させる室内機熱交換器5と、この室内機熱交換器の風路6 Aの一次側に設けられた自然蒸発式加湿器9とを有する室内機Bを備えた構成とする。



【特許請求の範囲】

【請求項1】 圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、上記圧縮機の吸入側に接続されたアキュムレータとを有する室外機、及び上記室外機熱交換器からの液化冷媒を減圧する絞り装置と、利用側で所定の風路中に配設され、上記絞り装置によって減圧された冷媒を蒸発させてガス化し、上記アキュムレータに流入させる室内機熱交換器と、上記室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器とを有する室内機を備えたことを特徴とする空気調和装置。

【請求項2】 上記室内機熱交換器は、冷媒入口が風路の二次側に位置し、冷媒出口が風路の一次側に位置するように配設されたことを特徴とする請求項1記載の空気調和装置。

【請求項3】 上記室内機熱交換器の管外伝熱面積を、蒸発温度が高くても十分な冷却能力が確保できる程度に大きくすることを特徴とする請求項1または請求項2記載の空気調和装置。

【請求項4】 上記圧縮機を容量可変型の圧縮機としたことを特徴とする請求項1～請求項3のいずれか1項記載の空気調和装置。

【請求項5】 上記室内機熱交換器の液側温度が所定温度以上となるように圧縮機を容量制御する制御装置を備えたことを特徴とする請求項4記載の空気調和装置。

【請求項6】 上記所定温度は、露点温度であることを特徴とする請求項5記載の空気調和装置。

【請求項7】 上記露点温度は、室内機熱交換器の吸込空気温度から一定温度を差し引くことにより算出した液温度下限値を対応させるようにしたことを特徴とする請求項6記載の空気調和装置。

【請求項8】 上記露点温度は、室内機熱交換器の吸込空気温度と湿度にもとづいて算出するようにしたことを特徴とする請求項6記載の空気調和装置。

【請求項9】 圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、上記圧縮機の吸入側に接続されたアキュムレータとを有する2台の室外機、各室外機にそれぞれ接続され液冷媒を減圧する第1及び第2の絞り装置と、第1、第2の絞り装置にそれぞれ接続され減圧された冷媒を蒸発させてガス化し、各室外機のアキュムレータにそれぞれ流入させ、2つの冷媒回路を構成する第1及び第2の室内機熱交換器と、上記各室内機熱交換器に対して熱交換用の風路を形成する送風手段とを有する1台の室内機、及び上記各室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器を備えたことを特徴とする空気調和装置。

【請求項10】 圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、上記圧縮機の吸入側に接続されたアキュムレータとを有する2台の室外機、各室外機にそれぞれ接続され液冷媒を減圧する

第1及び第2の絞り装置と、第1、第2の絞り装置にそれぞれ接続され減圧された冷媒を蒸発させてガス化し、各室外機のアキュムレータにそれぞれ流入させ、2つの冷媒回路を構成する第1及び第2の室内機熱交換器と、上記各室内機熱交換器に対して熱交換用の風路を形成する送風手段とを有する1台の室内機、上記第1の室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器、及び上記第1の室内機熱交換器の蒸発温度を第2の室内機熱交換器の蒸発温度より高く制御する制御装置を備えたことを特徴とする空気調和装置。

【発明の詳細な説明】

【0001】

【発明の属する技術分野】この発明は、空気調和装置、特に電算機室のように、年間を通じて冷房空調を行なう空気調和装置に関するものである。

【0002】

【従来の技術】従来の電算機室における年間冷房空調装置の圧縮機は固定容量であるため、低負荷時には再熱を行ない能力調整を行っていた。その際、過大な除湿を伴うため、湿度管理のために強制的に加湿を行なう周知のペーパーパン方式の加湿器を利用していた。

【0003】

【発明が解決しようとする課題】ペーパーパン方式によって強制的に加湿を行なう従来の空気調和装置においては、常に電力を必要とするため消費電力が増加するという問題点があった。また、ペーパーパン方式では定期的にメンテナンスを実施しないと加湿能力の低下や空気調和装置の内部が汚れるという問題点があった。加湿器として消費電力が不要で清掃が容易な自然蒸発式加湿器を利用するとしても、自然蒸発式加湿器を通過する空気の温度が低いため十分な加湿能力を発揮することができず実用化は困難であった。

【0004】この発明は、上記のような問題点を解決するためになされたもので、年間を通じて冷房空調を行なう場合において、自然蒸発式加湿器を圧縮機の容量制御により効率的に利用することができる空気調和装置を得ることを目的とする。

【0005】

【課題を解決するための手段】この発明に係る空気調和装置は、圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、圧縮機の吸入側に接続されたアキュムレータとを有する室外機、及び室外機熱交換器からの液化冷媒を減圧する絞り装置と、利用側で所定の風路中に配設され、絞り装置によって減圧された冷媒を蒸発させてガス化し、アキュムレータに流入させる室内機熱交換器と、この室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器とを有する室内機を備えたものである。

【0006】この発明に係る空気調和装置は、また、室内機熱交換器の冷媒入口を風路の二次側に位置させ、冷

媒出口を風路の一次側に位置させるように配設したものである。

【0007】この発明に係る空気調和装置は、また、室内機熱交換器の管外伝熱面積を、蒸発温度が高くて十分な冷却能力が確保できる程度に大きくするものである。

【0008】この発明に係る空気調和装置は、また、圧縮機を容量可変型の圧縮機としたものである。

【0009】この発明に係る空気調和装置は、また、室内機熱交換器の液側温度が所定温度以上となるように圧縮機を容量制御する制御装置を備えたものである。

【0010】この発明に係る空気調和装置は、また、所定温度を露点温度としたものである。

【0011】この発明に係る空気調和装置は、また、露点温度として室内機熱交換器の吸込空気温度から一定温度を差し引くことにより算出した液温度下限値を対応させるようにしたものである。

【0012】この発明に係る空気調和装置は、露点温度を室内機熱交換器の吸込空気温度と湿度にもとづいて算出するようにしたものである。

【0013】この発明に係る空気調和装置は、また、圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、圧縮機の吸入側に接続されたアキュムレータとを有する2台の室外機、各室外機にそれぞれ接続され液冷媒を減圧する第1及び第2の絞り装置と、第1、第2の絞り装置にそれぞれ接続され減圧された冷媒を蒸発させてガス化し、各室外機のアキュムレータにそれぞれ流入させ、2つの冷媒回路を構成する第1及び第2の室内機熱交換器と、各室内機熱交換器に対して熱交換用の風路を形成する送風手段とを有する1台の室内機、及び各室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器を備えたものである。

【0014】この発明に係る空気調和装置は、また、圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、圧縮機の吸入側に接続されたアキュムレータとを有する2台の室外機、各室外機にそれぞれ接続され液冷媒を減圧する第1及び第2の絞り装置と、第1、第2の絞り装置にそれぞれ接続され減圧された冷媒を蒸発させてガス化し、各室外機のアキュムレータにそれぞれ流入させて2つの冷媒回路を構成する第1及び第2の室内機熱交換器と、各室内機熱交換器に対して熱交換用の風路を形成する送風手段とを有する1台の室内機、第1の室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器、及び第1の室内機熱交換器の蒸発温度を第2の室内機熱交換器の蒸発温度より高く制御する制御装置を備えたものである。

【0015】

【発明の実施の形態】実施の形態1. 以下、この発明の実施の形態1を図にもとづいて説明する。図1は、実施の形態1の構成を示す冷媒回路図である。この図におい

て、Aは室外機で、以下に述べる各装置によって構成されている。即ち、1は容量可変型の圧縮機、2は室外機熱交換器、3は室外機熱交換器2に設けられた室外機送風手段、4は絞り装置、5は室内機熱交換器、6は室内機熱交換器5に設けられた室内機送風手段で、動作時に矢印6Aで示す風路を形成する。7はアキュムレータ、8は上記各装置を上記の順に直列に接続し、冷媒回路を構成する冷媒配管、9は室内機熱交換器5の風路6Aの1次側に設けられた自然蒸発式の加湿器、10は室内機熱交換器5の風路の吸込み側（1次側）に設けられた吸込み空気温度検知器、11は同じく吹出し側（2次側）に設けられた吹出し空気温度検知器、12は室内機熱交換器5の入口近傍に設けられた液側温度検知器、13は同じく出口近傍に設けられたガス側温度検知器、14は上記各温度検知器の検知結果にもとづいて絞り装置4を含む室内機Bを制御する室内機制御装置、15は室外機Aに設けられ圧縮機1を容量制御する室外機制御装置、16は利用側に設けられ室内機制御装置14及び室外機制御装置15を制御する利用側制御装置である。

【0016】次に、実施の形態1の空気調和装置の冷媒の流れについて説明する。圧縮機1から吐出される高温、高圧のガス冷媒は、室外機熱交換器2へ流入し、室外機送風手段3の送風を含む常温の空気などにより冷却されて凝縮液化する。室外機熱交換器2を出た冷媒は絞り装置4で減圧され、室内機熱交換器5へ流入する。室内機熱交換器5で低温を発生すると共に、冷媒は蒸発しガス化して流出し、ガス冷媒がアキュムレータ7へ流入し、通過した後、圧縮機1へ吸入される。

【0017】次に、絞り装置4の制御について図2のフローチャートを用いて説明する。まず、ステップS1で室内機熱交換器5の液側温度検知器12の検出温度 TH_1 と、ガス側温度検知器13の検出温度 TH_2 との差であるスーパーヒート $SH (= TH_2 - TH_1)$ を算出する。次に、ステップS2でスーパーヒート SH と目標スーパーヒート値 SH_m との大小比較により絞り装置4を絞るか開けるかを判断する。 $SH > SH_m$ の場合には、ステップS3で絞り装置4の開き量 $S_j 2 (SH)$ を算出し、ステップS4で $S_j 2 (SH)$ だけ絞り装置4を開く。また、ステップS2で $SH < SH_m$ の場合には、ステップS5で絞り装置4の絞り量 $S_j 1 (SH)$ を算出し、ステップS6で $S_j 1 (SH)$ だけ絞り装置4を絞る。

【0018】次に、加湿器9について説明する。加湿器9は電力供給の不要な、透質膜式を含む自然蒸発式の加湿方式を採用したものであり、加湿器9を通過する空気の温度、湿度、風量により加湿性能が変化する。即ち、高温、低湿、大風量であるほど加湿性能が向上し、逆の場合は加湿性能が低下するため、自動的に湿度調整が行なえる。ここで、加湿器9を室内機熱交換器5の風路6Aの2次側に設置すると、加湿器9を通過する空気が低

温多湿の空気となって加湿効率が非常に低下するため、実施の形態1では、加湿器を室内機熱交換器5の風路6Aの1次側に設置し、加湿器9を通過する空気が、温度が高く低湿な室内機吸込み空気となるようにしている。こうして加湿器9により加湿された空気は、室内機熱交換器5により冷やされて室内空間に吹出される。このとき、室内機熱交換器5の液側温度が加湿器により加湿された空気の露点温度よりも低い場合には、一部凝縮して除湿されるため、圧縮機1を容量制御することにより、液側温度が露点温度よりも高くなるようにして、除湿されることなく室内空間に湿度を供給し得るようにしている。

【0019】自然蒸発式加湿器9は強制式の加湿器よりも加湿量が小さいが、容量制御可能な圧縮機1により除湿量を小さく抑えることができるため、過大な加湿は不要となる。特に、夏季や中間期においては、換気により室内に導入された外気は湿度が高いため加湿は不要である。また、冬季において、換気により室内に導入された外気は湿度が低いため加湿が必要となるが、電算機室等の対物空調においては、空調対象の室内での人の数が少ないため換気量は少なくてもよく、自然蒸発式加湿器の加湿量でも十分である。

【0020】次に、圧縮機1の制御の流れについて図3を用いて説明する。ステップS11で利用側制御装置16により設定された吹出し空気温度の目標温度TH4mと吹出し空気温度検知器11で検出された吹出し空気温度TH4とを比較する。TH4の方が大きい場合は、ステップS12で室内機熱交換器5の液側温度の目標値TH1mを小さくし、TH4の方が小さい場合は、ステップS13でTH1mを大きくする。次に、ステップS14で室内機吸込み空気温度検知器10の検出温度TH3と所定温度、例えば12℃との差を露点温度に対応する液側温度下限値TH1LMT(=TH3-12)として算出する。ステップS15でTH1mがTH1LMTよりも小さいときは、ステップS16でTH1m=TH1LMTとなるようにする。また、ステップS17で室内機熱交換器の液側温度検知器12の検出温度TH1がTH1mよりも大きいときは、ステップS18で圧縮機1の周波数を大きくして容量を増大させ、TH1がTH1mより小さいときは、ステップS19で圧縮機1の周波数を小さくして容量を小さくする。

【0021】低負荷時は圧縮機1の容量は小さく制御されるため、蒸発温度は高くなり顕熱比が1の状態で運転される。また、高負荷時は圧縮機1の容量は大きく制御され蒸発温度は低くなるが、多湿環境でなければ除湿量は少ない。加湿器9の加湿効率を上げるためには蒸発温度を上げて運転する必要がある。このように、室内機熱交換器5の中で最も温度の低い液側検出温度が露点温度よりも高くなるように圧縮機1の容量制御を行なうことで室内機熱交換器5での除湿量を0とすることが可能で

ある。

【0022】実施の形態1では、上述のように目標液温度TH1mを露点温度付近あるいはそれよりも高くするために、室内機吸込み空気温度-12として算出した液温度下限値TH1LMTを露点温度に対応する温度として制御を行なうようにしたが、湿度センサーを用いて吸込み空気温度検出値と湿度検出値とから露点温度を算出し、その値を目標液温度として制御するようにしてもよい。

【0023】また、室内機熱交換器5の容量を大きく、例えば管外伝熱面積を冷却能力28kWあたり70m²以上に設定することにより、蒸発温度が高くても冷房能力が十分に確保できるようにすることができる。

【0024】更に、室内機熱交換器5の冷媒パスを、冷媒入口側が熱交換器の風路6Aの2次側に位置するようにし、冷媒出口側が風路6Aの1次側に位置するように設定することによっても、蒸発温度が高くても冷房能力が十分に確保できるようにすることができる。

【0025】実施の形態2. 次に、この発明の実施の形態2を図にもとづいて説明する。図4は、実施の形態2の構成を示す冷媒回路図である。この図において、図1と同一または相当部分には同一符号を付して説明を省略する。図1と異なる点は、2台の室外機と、各室外機に対応した2つの室内機熱交換器を有する1台の室内機とによって構成され、2つの冷媒回路を形成するようにした点である。即ち、第1の冷媒回路100は、室内機Bの室内機熱交換器が第1の室内機熱交換器5となる点以外は図1と同じ構成とされている。また、第2の冷媒回路100Sは、室内機Bの第2の室内機熱交換器5Sに加湿器9が設けられていない点以外は第1の冷媒回路100と同じ構成とされている。第2の冷媒回路100Sを構成する各装置の符号は、第1の冷媒回路100の対応する装置の符号にSを付加して示し、個々の説明は省略する。なお、室内機Bの第1及び第2の室内機熱交換器5、5Sは、図示のように、おおむねV字形に配設され、室内機送風手段6は両室内機熱交換器5、5Sの中間位置の上部に吸込み型ファンとして設けられ、矢印6Aあるいは6ASのような風路を形成するようにされている。

【0026】次に、実施の形態2の冷媒の流れについて説明する。第1及び第2の冷媒回路100、100Sの冷媒の流れは同一であるため、第1の冷媒回路100についてのみ説明する。圧縮機1から吐出される高温、高圧のガス冷媒は、室外機熱交換器2へ流入し、室外機送風手段3の送風を含む常温の空気などにより冷却されて凝縮液化する。室外機熱交換器2を出た冷媒は絞り装置4で減圧され、第1の室内機熱交換器5へ流入する。第1の室内機熱交換器5で低温を発生すると共に、冷媒は蒸発しガス化して流出し、ガス冷媒がアキュムレータ7へ流入し、通過した後、圧縮機1へ吸入される。

【0027】絞り装置4の制御については、第1、第2の冷媒回路ともに実施の形態1と同様であるため説明を省略する。また、加湿器9については、第1の室内機熱交換器5にのみ配設されているが、その機能は実施の形態1と同様であるため説明を省略する。

【0028】次に、圧縮機1の制御の流れについて説明する。第1の冷媒回路100については実施の形態1と同様であるため説明を省略し、第2の冷媒回路100Sの圧縮機1の制御の流れについて図5を用いて説明する。ステップS21で利用側制御装置16により設定された吹出し空気温度の目標温度 $TH4$ よりも 1°C 低い値と吹出し空気温度検知器11で検出した吹出し空気温度 $TH4$ とを比較する。 $TH4$ の方が大きい場合は、ステップS22で第2の室内機熱交換器5Sの液側温度の目標値 $TH1m$ を小さくし、 $TH4$ の方が小さい場合は、ステップS23で $TH1m$ を大きくする。室内機吸込み空気温度検知器の検出温度 $TH3$ と所定温度、例えば 12°C との差を露点温度に対応する液側温度 $TH1\text{LMT}$ ($=TH3-12$) として算出する。ステップS25で $TH1m$ が $TH1\text{LMT}$ よりも小さいときは、ステップS26で $TH1m=TH1\text{LMT}$ となるようにする。また、ステップS27で室内機熱交換器の液側温度検知器12Sの検出温度 $TH1$ が $TH1m$ よりも大きいときは、ステップS28で圧縮機1Sの周波数を大きくして容量を増大させ、 $TH1$ が $TH1m$ より小さいときは、ステップS29で圧縮機1Sの周波数を小さくして容量を小さくする。

【0029】なお、第1の冷媒回路100と第2の冷媒回路100Sとは、図5中のステップS21のみが異なり、加湿器9を設けている第1の冷媒回路100よりも加湿器を設けていない第2の冷媒回路100Sの目標温度を低く読み替えることにより、第1の冷媒回路100よりも圧縮機1Sの容量を小さく制御する結果、第2の冷媒回路100Sの第2の室内機熱交換器5Sの蒸発温度を高くして加湿器9の加湿効率を上昇させることができる。更に、低負荷時は圧縮機の容量は小さく制御されるため、蒸発温度は高くなり顕熱比が1の状態で運転される。

【0030】このように、室内機熱交換器の中で最も温度の低い液側検出温度が露点温度よりも高くなるように圧縮機の容量制御を行なうことで室内機熱交換器での除湿量を0とすることが可能である。

【0031】実施の形態2では、目標液温度 $TH1m$ を露点温度付近あるいはそれより高くするために、室内機吸込み空気温度 -12 として算出した液温度下限値 $TH1\text{LMT}$ を露点温度に対応する温度として制御を行なうようにしたが、湿度センサーを用いて、吸込み空気温度検出値と湿度検出値とから露点温度を算出し、その値を目標液温度として制御してもよい。

【0032】また、室内機熱交換器の容量を大きく、例

えば管外伝熱面積を冷却能力 28 kW あたり 70 m^2 以上に設定することにより、蒸発温度が高くても冷房能力が十分に確保できるようにすることができる。

【0033】更に、室内機熱交換器の冷媒パスを、冷媒入口側が熱交換器の風路の2次側に位置するようにし、冷媒出口側が風路の1次側に位置するように設定することによっても、蒸発温度が高くても冷房能力が十分に確保できるようにすることができる。

【0034】なお、実施の形態2では、2つの冷媒回路を構成する場合について説明したが、3つ以上の冷媒回路を構成するようにしても、同様な効果を期待することができる。

【0035】

【発明の効果】この発明に係る空気調和装置は、圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、圧縮機の吸入側に接続されたアキュムレータとを有する室外機、及び室外機熱交換器からの液化冷媒を減圧する絞り装置と、利用側で所定の風路中に配設され、絞り装置によって減圧された冷媒を蒸発させてガス化し、アキュムレータに流入させる室内機熱交換器と、この室内機熱交換器の風路の一次側に設けられた自然蒸発式加湿器とを有する室内機を備えたものであるため、低い消費電力と簡易なメンテナンスで加湿を行なうことができる。

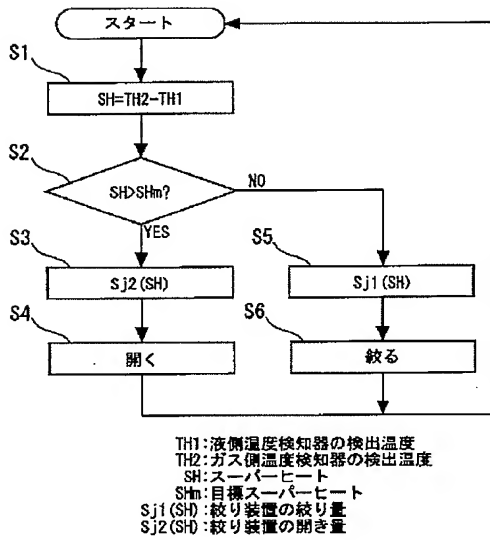
【0036】この発明に係る空気調和装置は、また、室内機熱交換器の冷媒入口を風路の二次側に位置させ、冷媒出口を風路の一次側に位置させるように配設した冷媒パス形状を有するため、冷房能力を損なうことなく室内機熱交換器の蒸発温度を高くすることができ、加湿器を効率良く利用することができる。

【0037】この発明に係る空気調和装置は、また、圧縮機を容量可変型の圧縮機としたものであるため、低い消費電力と簡易なメンテナンスで加湿を行なうことができる。

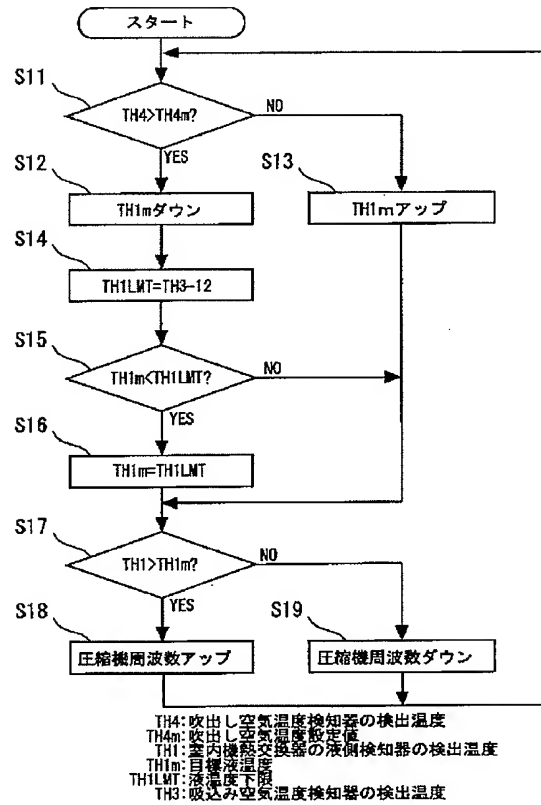
【0038】この発明に係る空気調和装置は、また、室内機熱交換器の液側温度が所定温度以上となるように圧縮機を容量制御する制御装置を備えたものであるため、室内機熱交換器の蒸発温度を高くすることができ、加湿器を効率良く利用することができる。

【0039】この発明に係る空気調和装置は、また、圧縮機と、この圧縮機から吐出されたガス冷媒を凝縮液化する室外機熱交換器と、圧縮機の吸入側に接続されたアキュムレータとを有する2台の室外機、各室外機にそれぞれ接続され液冷媒を減圧する第1及び第2の絞り装置と、第1、第2の絞り装置にそれぞれ接続され減圧された冷媒を蒸発させてガス化し、各室外機のアキュムレータにそれぞれ流入させ、2つの冷媒回路を構成する第1及び第2の室内機熱交換器と、各室内機熱交換器に対して熱交換用の風路を形成する送風手段とを有する1台の室内機、及び各室内機熱交換器の風路の一次側に設けら

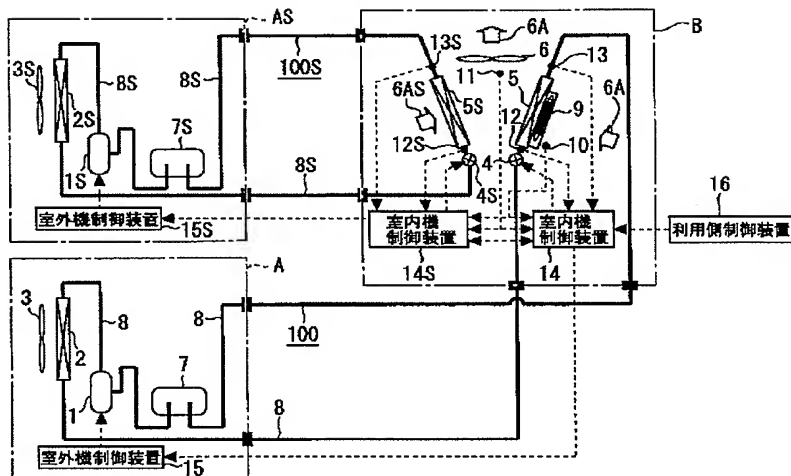
【図2】



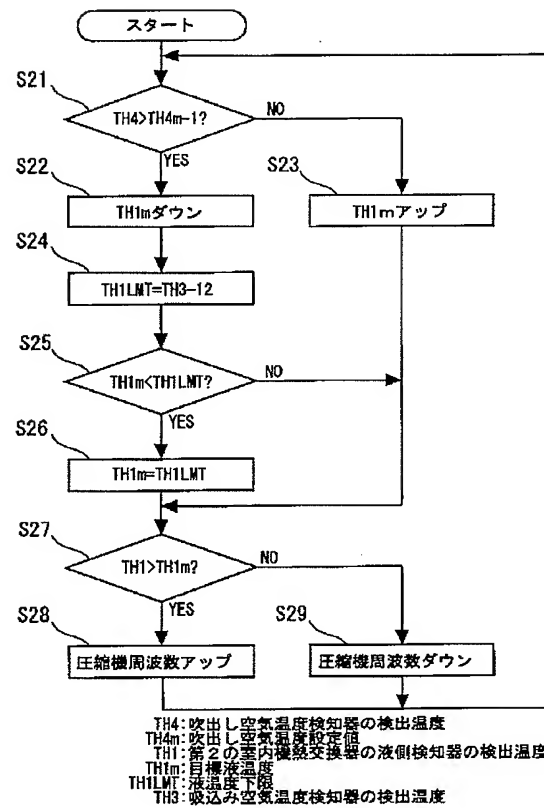
【図3】



【図4】



【図5】



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